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APPLICATION NO.	FILING DATE	FIRST NAMED INVENTOR	ATTORNEY DOCKET NO.	CONFIRMATION NO.
10/031,025	06/06/2002	Albertus Cornelis Den Brinker	NL 000288	4466

7590 02/18/2005  
Corporate Patent Counsel  
Philips Electronics North America Corporation  
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EXAMINER

VO, HUYEN X

ART UNIT	PAPER NUMBER
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2655

DATE MAILED: 02/18/2005

Please find below and/or attached an Office communication concerning this application or proceeding.

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## Office Action Summary

**Application No.**

10/031,025

**Applicant(s)**

DEN BRINKER ET AL.

**Examiner**

Huyen Vo

**Art Unit**

2655

– The MAILING DATE of this communication appears on the cover sheet with the correspondence address –

### Period for Reply

A SHORTENED STATUTORY PERIOD FOR REPLY IS SET TO EXPIRE 3 MONTH(S) FROM THE MAILING DATE OF THIS COMMUNICATION.

- Extensions of time may be available under the provisions of 37 CFR 1.136(a). In no event, however, may a reply be timely filed after SIX (6) MONTHS from the mailing date of this communication.
- If the period for reply specified above is less than thirty (30) days, a reply within the statutory minimum of thirty (30) days will be considered timely.
- If NO period for reply is specified above, the maximum statutory period will apply and will expire SIX (6) MONTHS from the mailing date of this communication.
- Failure to reply within the set or extended period for reply will, by statute, cause the application to become ABANDONED (35 U.S.C. § 133). Any reply received by the Office later than three months after the mailing date of this communication, even if timely filed, may reduce any earned patent term adjustment. See 37 CFR 1.704(b).

### Status

- 1) ☒ Responsive to communication(s) filed on 06 June 2002.
- 2a) ☐ This action is **FINAL**. 2b) ☒ This action is non-final.
- 3) ☐ Since this application is in condition for allowance except for formal matters, prosecution as to the merits is closed in accordance with the practice under *Ex parte Quayle*, 1935 C.D. 11, 453 O.G. 213.

### Disposition of Claims

- 4) ☒ Claim(s) 1-7 is/are pending in the application.
- 4a) Of the above claim(s) \_\_\_\_\_ is/are withdrawn from consideration.
- 5) ☐ Claim(s) \_\_\_\_\_ is/are allowed.
- 6) ☒ Claim(s) 1-7 is/are rejected.
- 7) ☐ Claim(s) \_\_\_\_\_ is/are objected to.
- 8) ☐ Claim(s) \_\_\_\_\_ are subject to restriction and/or election requirement.

### Application Papers

- 9) ☐ The specification is objected to by the Examiner.
- 10) ☒ The drawing(s) filed on 06 June 2002 is/are: a) ☒ accepted or b) ☐ objected to by the Examiner.  
Applicant may not request that any objection to the drawing(s) be held in abeyance. See 37 CFR 1.85(a).  
Replacement drawing sheet(s) including the correction is required if the drawing(s) is objected to. See 37 CFR 1.121(d).
- 11) ☐ The oath or declaration is objected to by the Examiner. Note the attached Office Action or form PTO-152.

### Priority under 35 U.S.C. § 119

- 12) ☐ Acknowledgment is made of a claim for foreign priority under 35 U.S.C. § 119(a)-(d) or (f).
- a) ☐ All b) ☐ Some \* c) ☐ None of:
1. ☐ Certified copies of the priority documents have been received.
  2. ☐ Certified copies of the priority documents have been received in Application No. \_\_\_\_\_.
  3. ☐ Copies of the certified copies of the priority documents have been received in this National Stage application from the International Bureau (PCT Rule 17.2(a)).
- \* See the attached detailed Office action for a list of the certified copies not received.

### Attachment(s)

- 1) ☒ Notice of References Cited (PTO-892)
- 2) ☐ Notice of Draftsperson's Patent Drawing Review (PTO-948)
- 3) ☒ Information Disclosure Statement(s) (PTO-1449 or PTO/SB/08)  
Paper No(s)/Mail Date 6/6/02.
- 4) ☐ Interview Summary (PTO-413)  
Paper No(s)/Mail Date. \_\_\_\_\_
- 5) ☐ Notice of Informal Patent Application (PTO-152)
- 6) ☐ Other: \_\_\_\_\_

## DETAILED ACTION

### *Claim Rejections - 35 USC § 102*

1. The following is a quotation of the appropriate paragraphs of 35 U.S.C. 102 that form the basis for the rejections under this section made in this Office action:

A person shall be entitled to a patent unless – (b) the invention was patented or described in a printed publication in this or a foreign country or in public use or on sale in this country, more than one year prior to the date of application for patent in the United States.

(e) the invention was described in (1) an application for patent, published under section 122(b), by another filed in the United States before the invention by the applicant for patent or (2) a patent granted on an application for patent by another filed in the United States before the invention by the applicant for patent, except that an international application filed under the treaty defined in section 351(a) shall have the effects for purposes of this subsection of an application filed in the United States only if the international application designated the United States and was published under Article 21(2) of such treaty in the English language.

2. Claims 1, 3, and 5-6 are rejected under 35 U.S.C. 102(b) as being anticipated by Eatwell (US Patent No. 5742694).

3. Regarding claims 1, 3, and 5, Eatwell discloses a method of encoding an audio signal, an audio encoder and system; comprising the steps of:

determining basic waveforms in the audio signal (*Predictable Component 3 in figure 4*);

obtaining a noise component from the audio signal by subtracting the basic waveforms from the audio signal (*Prediction Error 4 in figure 4*);

modeling a spectrum of the noise component by determining auto-regressive and moving-average parameters (*element 42 in figures 3 or 5, or referring to col. 8, ln. 22-47, where filter coefficients are determined*); and

including the auto-regressive and the moving-average parameters

and waveform parameters representing the basic waveforms in an encoded audio signal (*Output signal 8 in figures 3 or 5*).

4. Regarding claim 6, Eatwell discloses an encoded audio signal comprising:  
waveform parameters representing basic waveforms (*Predictable Component 3 in figure 4*); and

auto-regressive parameters and moving-average parameters representing a spectrum of a remaining noise component (*element 42 in figures 3 or 5 or referring to col. 8, ln. 22-47*).

5. Claims 1-6 are rejected under 35 U.S.C. 102(e) as being anticipated by Miseki et al. (US Patent No. 6167375).

6. Regarding claims 1, 3, and 5, Miseki et al. disclose a method of encoding an audio signal, an audio encoder and system, comprising the steps of:

determining basic waveforms in the audio signal (*Predictor 547 in figure 18*);  
obtaining a noise component from the audio signal by subtracting the basic waveforms from the audio signal (*Output of the summer 543 in figure 18*);

modeling a spectrum of the noise component by determining auto-regressive and moving-average parameters (*col. 8, ln. 22-47, where filter coefficients are determined*); and

including the auto-regressive and the moving-average parameters

and waveform parameters representing the basic waveforms in an encoded audio signal (*Output signal 513 in figure 16*).

7. Regarding claim 6, Miseki et al. discloses an encoded audio signal comprising:  
waveform parameters representing basic waveforms (*Predictor 547 in figure 18*);  
and auto-regressive parameters and moving-average parameters representing a  
spectrum of a remaining noise component (*col. 8, ln. 22-47, filter coefficients are  
determined*).

8. Regarding claims 2, 4, and 5, Miseki et al. disclose a method of decoding an  
encoded audio signal, an audio player and system, comprising the steps of:  
receiving an encoded audio signal comprising waveform parameters  
representing basic waveforms and auto-regressive and moving-average parameters  
representing a spectrum of a remaining noise component (*col. 23, ln. 1-35 together with  
figure 20, ARMA parameters are transmitted to the decoder side for use*);  
filtering a white noise signal to obtain a reconstructed noise component, which  
filtering is determined by the auto-regressive parameters and the moving-average  
parameters (*Noise Decoder 290 in figure 23*);  
synthesizing basic waveforms based on the waveform parameters (*Speech  
Decoder 280 in figure 23*); and  
adding the reconstructed noise component to the synthesized basic waveforms  
to obtain a decoded audio signal (*Mixer 295 in figure 23*).

***Claim Rejections - 35 USC § 103***

9. The following is a quotation of 35 U.S.C. 103(a) which forms the basis for all obviousness rejections set forth in this Office action:

(a) A patent may not be obtained though the invention is not identically disclosed or described as set forth in section 102 of this title, if the differences between the subject matter sought to be patented and the prior art are such that the subject matter as a whole would have been obvious at the time the invention was made to a person having ordinary skill in the art to which said subject matter pertains. Patentability shall not be negated by the manner in which the invention was made.

10. Claim 7 is rejected under 35 U.S.C. 103(a) as being unpatentable over Eatwell (US Patent No. 5742694).

11. Regarding claim 7, Eatwell fails to disclose a storage medium on which an encoded audio signal as claimed in claim 6 is stored. However, it would have been obvious to one skilled in the art at the time of invention to implement the method in claim 6 in computer codes to facilitate maintenance and updating.

12. Claim 7 is rejected under 35 U.S.C. 103(a) as being unpatentable over Miseki et al. (US Patent No. 6167375).

13. Regarding claim 7, Miseki et al. fail to disclose a storage medium on which an encoded audio signal as claimed in claim 6 is stored. However, it would have been obvious to one skilled in the art at the time of invention to implement the method in claim 6 in computer codes to facilitate maintenance and updating.

**Conclusion**

The prior art made of record and not relied upon is considered pertinent to applicant's disclosure. *Akamine* et al. (IEEE Publication) teach an ARMA model based speech coding scheme that is considered pertinent to the claimed invention.

Any inquiry concerning this communication or earlier communications from the examiner should be directed to Huyen Vo whose telephone number is 703-305-8665. The examiner can normally be reached on M-F, 9-5:30.

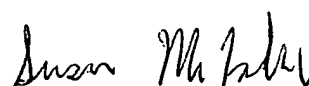
If attempts to reach the examiner by telephone are unsuccessful, the examiner's supervisor, Doris To can be reached on 703-305-4827. The fax phone number for the organization where this application or proceeding is assigned is 703-872-9306.

Information regarding the status of an application may be obtained from the Patent Application Information Retrieval (PAIR) system. Status information for published applications may be obtained from either Private PAIR or Public PAIR. Status information for unpublished applications is available through Private PAIR only. For more information about the PAIR system, see <http://pair-direct.uspto.gov>. Should you have questions on access to the Private PAIR system, contact the Electronic Business Center (EBC) at 866-217-9197 (toll-free).

Examiner Huyen X. Vo

November 22, 2004

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SUSAN MCFADDEN  
PRIMARY EXAMINER



Form PTO-1449 COMMERCE (REV. 7-80)		DEPARTMENT OF PATENT AND TRADEMARK OFFICE		Atty. Docket No. NL 000288		Serial No. 10/031,025	
INFORMATION DISCLOSURE CITATION (Use several sheets if necessary)				Applicant  ALBERTUS C. DEN BRINKER ET AL.			
				Filing Date 1/14/02		Group	
U.S. PATENT DOCUMENTS							
Ex. Int		Document Number	Date	Name	Class	Sub- class	Filing Date If Approp.
	AA						
	AB						
	AC						
	AD						
	AE						
	AF						
FOREIGN PATENT DOCUMENTS							
		Document Number	Date	Country	Class	Sub- class	Trans. Yes No
	AG						
	AH						
	AI						
	AJ						
	AK						
OTHER (Including Author, Title, Date, Pertinent Pages, Etc.)							
	AL	Petre Stoica et al., "Introduction to Spectral Analysis," Prentice-Hall Inc., 1997, pages 101-108.					
	AM						
	AN						
Examiner <i>Huyen X VO</i>				Date Considered <i>11/22/00</i>			
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Form PTO-1449 COMMERCE (REV. 7-80)		U.S. DEPARTMENT OF PATENT AND TRADEMARK OFFICE		Atty. Docket No. NL 000288		Serial No. <b>10/031025</b>										
<b>INFORMATION DISCLOSURE CITATION</b> (Use several sheets if necessary)				Applicant <b>ALBERTUS C. DEN BRINKER ET AL.</b>												
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<b>U.S. PATENT DOCUMENTS</b>																
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<b>Notice of References Cited</b>	Application/Control No. 10/031,025	Applicant(s)/Patent Under Reexamination DEN BRINKER ET AL.	
	Examiner Huyen Vo	Art Unit 2655	Page 1 of 1

**U.S. PATENT DOCUMENTS**

*		Document Number Country Code-Number-Kind Code	Date MM-YYYY	Name	Classification
	A	US-5,742,694	04-1998	Eatwell, Graham P.	381/94.2
	B	US-6,167,375	12-2000	Miseki et al.	704/229
	C	US-			
	D	US-			
	E	US-			
	F	US-			
	G	US-			
	H	US-			
	I	US-			
	J	US-			
	K	US-			
	L	US-			
	M	US-			

**FOREIGN PATENT DOCUMENTS**

*		Document Number Country Code-Number-Kind Code	Date MM-YYYY	Country	Name	Classification
	N					
	O					
	P					
	Q					
	R					
	S					
	T					

**NON-PATENT DOCUMENTS**

*		Include as applicable: Author, Title Date, Publisher, Edition or Volume, Pertinent Pages)
	U	Akamine, M.; Miseki, K., "ARMA model based speech coding at 8 kb/s" Acoustics, Speech, and Signal Processing, 1989. ICASSP-89., 1989 International, Conference on , 23-26 May 1989, Pages:148 - 151 vol.1
	V	
	W	
	X	

\*A copy of this reference is not being furnished with this Office action. (See MPEP § 707.05(a).)  
Dates in MM-YYYY format are publication dates. Classifications may be US or foreign.

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## ABSTRACT

This paper proposes a new speech coding for high quality performance at 8 kbps. The coder is based on an ARMA model as the prediction filter and a new excitation model. A simple ARMA analysis method is proposed. This analysis method features a technique for eliminating the fine harmonic structure within the speech spectrum. This overcomes the problem of MA parameter misestimation. The excitation signal is modeled as a pulse train whose density is varied depending on the residual signal's power. The proposed coder produced high quality speech comparable with 6-bit log PCM at 8 kbps according to computer simulation.

## 1. INTRODUCTION

Various speech coding methods at bit rate below 10 kbps have been proposed for applications to private communication networks and mobile systems. A class of methods, adaptive predictive coding (APC) [1][2], multi pulse coding (MPC) [3][4], and code excited linear prediction coding (CELP) [5] seems to be promising for these applications. This class of methods represents a speech spectral envelope as an all pole model, in other words, an AR model. However there are not only poles but also zeros in speech spectra. Especially, nasal and consonant sounds tend to have spectral zeros. The AR model is less satisfactory in describing these zeros accurately. An ARMA model can be attractive for improving speech quality in low bit rate speech coding because of its ability to describe both spectral poles and zeros efficiently. However, the ARMA model has rarely been used in speech coding so far, because the resulting estimation problem in an ARMA based system is a non-linear problem.

Ishizaki proposed a simple ARMA analysis method [6]. In the method, the AR and MA parameters are obtained separately. The AR parameters are determined by LPC analysis using the autocorrelation method. The MA parameters are obtained by inverting the power spectrum of the AR model's residual signal, and applying LPC analysis to the corresponding autocorrelation function. This ARMA estimation method requires LPC analysis and FFT. Therefore, the method has low computational complexity. But, the method often fails to estimate the MA parameters because of the fine harmonic structure within speech spectra. Thus, a technique for eliminating the fine harmonic structure in the frequency domain and the time domain has been considered here.

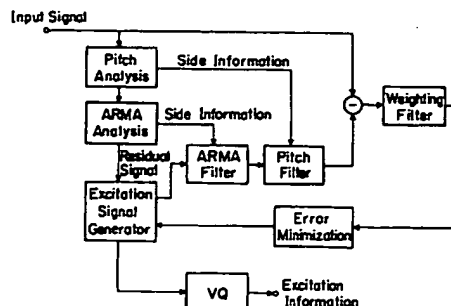


Fig. 1 Block diagram of the proposed coding algorithm.

The authors propose a new ARMA model based speech coder. The proposed coder includes a pitch filter, an ARMA filter, and an excitation signal model. The excitation signal is modeled as a pulse train whose density is varied depending on the residual signal's power. The ARMA residual signal is divided into several subframe signals in the time domain. The excitation signal is represented by closely spaced pulses in subframes with large residual power, while the excitation signal is represented by more widely spaced pulses in the subframes with low residual power. Each subframe's excitation is determined analytically to minimize the perceptually weighted errors between original and synthetic signals.

## 2. CODING ALGORITHM

Figure 1 shows a block diagram of the proposed coder. The coder consists of two parts. The first part includes a pitch filter and an ARMA filter. The second part is an excitation signal generator. The pitch filter generates the pitch periodicity of voiced speeches. The ARMA filter restores the spectral envelope. The excitation signal is modeled as adaptive density pulses (ADP). Its amplitude is quantized with a vector quantizer. The pitch parameters, the ARMA parameters and the ADP's density and phase are transmitted to the receiver as side information. The coder will be called ARMA-ADP in this paper.

## A. ARMA ANALYSIS

The proposed analysis method is depicted in Fig. 2. In this method, the AR and MA parameters are estimated separately. The well known LPC analysis method is used for estimating the AR

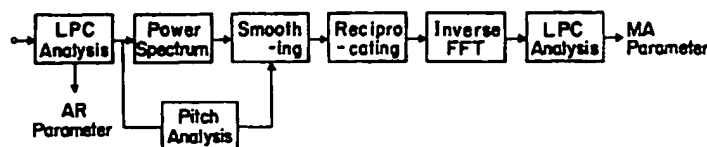


Fig. 2 Block diagram of the proposed ARMA analysis method.

parameters. After converting spectral zeros to poles, LPC analysis is applied to obtain the MA parameters. Zero-to-pole conversion is accomplished as follows. First, the power spectrum of the AR residual signal is calculated by FFT. Then the power spectrum is filtered in the frequency domain to remove its spectral harmonic structure. This filtering is equivalent to spectrum smoothing. The proposed ARMA analysis has a feature in the method for removing the harmonic structure. If we fail to remove it, the MA parameters are misestimated, because the deep valleys of the harmonic structure are changed to acute peaks in the zero-to-pole conversion.

The authors considered the ways for eliminating the fine harmonic structure. Voiced speech waveforms are quasi periodic, not strictly periodic. However, for the sake of simple explanation, voiced speech is assumed to be strictly periodic signal with a pitch period  $T_p[s]$ . Then, the speech spectra are frequency-discrete. Considering the Fourier transform of the discrete spectra, the Fourier representation is a periodic function with a period  $T_p$ . A continuous spectrum can be obtained by using an ideal lowpass filter with a  $T_p/2$  bandwidth. Therefore, the frequency characteristic of the filter must change adaptively depending on the pitch period. Also, the filter must have a zero-phase characteristic. Spectrum zeros will be shifted unless the filter is zero-phase. It should be noticed that a filter closely approximating an ideal lowpass filter is computationally expensive because the resulting filter is of a high order. A low order filter causes less distortion in the spectral envelope because the autocorrelation function  $r(k)$  of the AR residual signal decreases rapidly with  $k$ .

Thus, in order to remove the fine structure, a first-order IIR filter was used whose coefficient is adaptively varied so that the filter's time constant is proportional to the interval of the pitch harmonics. Let  $N$  be the order of FFT and  $T$  [sample] the pitch period. The filter's coefficient  $a$  is described as a function of the pitch period as follows.

$$a = \exp(Nb/T) \quad (1)$$

where  $b$  is a constant which is experimentally determined. Filtering is accomplished toward two directions, forward and backward as follows.

$$D_f(k) = D(k) + a D_f(k-1) \quad k=1, 2, \dots, N \quad (2)$$

$$D_b(k) = D(k) + a D_b(k+1) \quad k=N, N-1, \dots, 1 \quad (3)$$

$$\bar{D}(k) = [D_f(k) + D_b(k)] / 2 \quad k=1, 2, \dots, N \quad (4)$$

where  $D_f(k)$ ,  $D_b(k)$ ,  $D(k)$  and  $\bar{D}(k)$  are the forward filtered spectrum, the backward filtered

spectrum, the power spectrum of the AR residual signal and the smoothed power spectrum, respectively. This makes the filter's phase characteristic zero-phase.

The operations described above are done in frequency domain. The power spectrum smoothing and the zero-to-pole conversion can also be carried out in the time domain. Spectrum smoothing is carried out by windowing the corresponding autocorrelation function with a rectangular window. Zero-to-pole conversion is performed as follows. Let  $D_r(k)$  be the reciprocal of the smoothed power spectrum  $\bar{D}(k)$ . Then

$$\bar{D}(k) \cdot D_r(k) = 1 \quad k=1, 2, \dots, N. \quad (5)$$

By the inverse Fourier transform of the above equation, we can obtain

$$\sum_{k=0}^{N-1} r(k) r'(n-k) = \delta(n) \quad n=0, 1, \dots, N-1 \quad (6)$$

where  $r(k)$  and  $r'(k)$  is the corresponding autocorrelation function of  $\bar{D}(k)$  and  $D_r(k)$ , respectively, and  $\delta(n)$  is the Kronecker delta function. This equation is rewritten as follows.

$$\begin{bmatrix} r(0) & r(1) & \dots & r(N-1) \\ r(1) & r(0) & \dots & r(N-2) \\ \vdots & \vdots & \ddots & \vdots \\ r(N-1) & r(N-2) & \dots & r(0) \end{bmatrix} \begin{bmatrix} r'(0) \\ r'(1) \\ \vdots \\ r'(N-1) \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{bmatrix} \quad (7)$$

The autocorrelation function  $r'(k)$  is obtained by resolving the above equation.

Comparing the operation in the time domain with the operation in the frequency domain from the viewpoint of computational complexity, the former is expensive. The computational complexity of the time domain operation is  $O(N^3)$ , while the computational complexity of the frequency domain operation is  $O(N \log_2 N)$ . What is worse that high precision is required to resolve equation (7).

Therefore, the frequency domain method was used.

## B. ADAPTIVE DENSITY PULSE MODEL

The authors propose adaptive density pulses (ADP) as the synthesis filter's excitation signal. An ADP is a pulse train which is located with a constant interval, namely, with a constant density in the subframe, but the density is different subframe by subframe. The ARMA residual signal is divided into several subframe signals in a coding frame. The ADP's density is set high when the subframe's power is high, while the ADP's density is set low when the subframe's power is low. The amplitudes of the ADP are analytically determined to minimize the perceptually weighted errors between the original and synthetic speech signals.

Let  $N$  be the coding frame length,  $L$  the subframe length, and  $M$  the number of subframes in the coding frame. The  $m$ 'th subframe's excitation signal  $v^{(m)}(n)$  is described as follows.

$$v^{(m)}(n) = \sum_{i=1}^{Q_m} g_i^{(m)} \delta(n-(i-1)D_m - K_m) \quad (8)$$

$$n=1, 2, \dots, L$$

$$1 \leq K_m \leq D_m$$

where  $D_m$ ,  $Q_m$ ,  $K_m$ , and  $g_i^{(m)}$  denotes the interval, number, phase, and amplitude of the ADP in the  $m$ 'th subframe, respectively. Superscript  $(m)$  denotes that the sequence with the superscript is defined only in the  $m$ 'th subframe. Time  $(n)$  is defined so as to be reset to one at each subframe's beginning. An example of ADP is shown in Fig.3. The synthesized signal  $y^{(m)}(n)$  is represented by the convolution between the synthesis filter's impulse response  $h(n)$  and the excitation signal  $v^{(m)}(n)$ .

$$y^{(m)}(n) = \sum_{j=1}^L v^{(m)}(j)h(n-j)$$

$$= \sum_{i=1}^{Q_m} g_i^{(m)} h[n-(i-1)D_m - K_m] \quad (9)$$

On the condition that  $D_m$  and  $Q_m$  are given, the amplitudes  $g_i^{(m)}$  and phase  $K_m$  of the  $m$ 'th subframe's ADP are determined so as to minimize the total squared error

$$E^{(m)} = \sum_{n=1}^L [S_w^{(m)}(n) - y_w^{(m)}(n)]^2, \quad (10)$$

where  $S_w^{(m)}(n)$  denotes the weighted speech signal after subtracting the contributions carried over from the previous coding frame and subframes, and  $y_w^{(m)}(n)$  denotes the weighted synthetic signal. After differentiating  $E$  in terms of the amplitudes  $g_i^{(m)}$  ( $i=1, 2, \dots, Q_m$ ), let them be zeros. Then the following equations hold.

$$\sum_{i=1}^{Q_m} g_i^{(m)} R_{hh}(I, J) = R_{sh}^{(m)}(J) \quad (11)$$

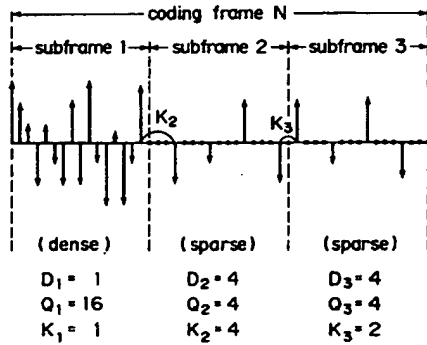


Fig.3 An example of ADP with  $N=48$  and  $L=16$ .

$$I=(i-1)D_m + K_m, J=(j-1)D_m + K_m$$

$$1 \leq i, j \leq Q_m$$

where  $R_{hh}(I, J)$  and  $R_{sh}^{(m)}(J)$  represents

$$\sum_{n=1}^L h_w(n-I)h_w(n-J)$$

and

$$\sum_{n=1}^L S_w^{(m)}(n)h_w(n-J),$$

respectively. The sequence  $h_w(n)$  denotes the weighted synthesis filter's impulse response. The  $D_m$  sets of candidates for the ADP's amplitudes are given by solving the equations (11) in terms of  $g_i^{(m)}$  for  $K_m = 1, 2, \dots, D_m$ . The  $D_m$  kinds of minimum squared errors of  $E^{(m)}(K_m)$  are represented by substituting Eq.(11) into Eq.(10).

$$E_{\min}^{(m)}(K_m) = \sum_{n=1}^L [S_w^{(m)}(n)]^2 - \sum_{i=1}^{Q_m} g_i^{(m)} R_{sh}^{(m)}(I) \quad (12)$$

$$I = (i-1)D_m + K_m$$

Therefore the optimum phase of the ADP can be set to such a  $K_m$  that maximizes the second summation on the right side of Eq.(12). The optimum amplitudes are chosen among the  $D_m$  sets of candidates from the optimum phase  $K_m$ . The perceptual weighting filter is represented by the ARMA synthesis filter  $H(Z)$  in the  $z$  transform domain by

$$W(Z) = H(rZ)/H(Z) \quad (13)$$

where  $0 \leq r \leq 1$ .

### 3. EXPERIMENTAL RESULTS

The inverse of the spectral flatness measure (sfm) [7] of the ARMA residual signals was calculated to evaluate the proposed ARMA analysis by computer simulations. The inverse of the sfm is a measure of waveform predictability [7]. Table 1 shows a segmental  $\text{sfm}^{-1}$  for the conventional ARMA analysis method (Method 0) and the proposed two methods, which are methods with means for eliminating the fine harmonic structure in the frequency domain (Method 1) and in the time domain (Method 2). The  $\text{sfm}^{-1}$  seg is an averaged inverse of the sfm in dB units. Speech samples used for the simulations were one short Japanese sentence uttered by two male and two female speakers. The analysis frame length, the AR order, and the MA order, was 256 samples, 8, and 4, respectively. From Table 1, it can be seen that the conventional method was improved by the proposed methods.

Table 1  $\text{Sfm}^{-1}_{\text{seg}}$  of the ARMA residual signal.

	Male 1	Male 2	Female 1	Female 2
Method 0	8.64	5.65	9.77	8.14
Method 1	5.07	4.08	5.97	4.79
Method 2	5.33	3.96	6.14	5.00

Computer simulations were conducted to evaluate the proposed ARMA-ADP coder's performance. Table 2 shows the coding parameters and the bit allocation for them. The coding frame length and subframe length were set to 240 and 40 samples at an 8 kHz sampling rate, respectively. Two kinds of densities for ADP were used, that is, the pulse interval was two samples for dense ADPs and four samples for sparse ADPs. The number of subframes where ADP was dense was two per coding frame. The AR parameters were quantized after being converted to a log-area ratio. The MA parameters were directly quantized. ADP was quantized by a vector quantizer (VQ). The codebook was designed with 30000 training vectors generated from real speech samples using the LBG algorithm. The speech samples used for subjective and objective tests were the same ones mentioned above. They were different from the speech samples used for the VQ's design.

Table 3 shows the segmental SNR for the proposed coder at 8 kbps. The synthetic speeches had high segmental SNRs, and they were high-quality and comparable with 6-bit log PCM.

Table 2 Coding parameters.

Bit rate	8 kbps
Sampling rate	8 kHz
Frame length	
Analysis	32 ms (256 samples)
Coding	30 ms (240 samples)
Pitch analysis	1 st order
Bit allocation	12 bits
ARMA analysis	AR 8th, MA 4th
Bit allocation	48 bits
ADP	
Subframe length	40 samples
Pulse interval	2 sample (2 subframe)
	4 samples (4 subframes)
VQ Dimension	5
Size	10 bits
Bit allocation	180 bits

#### 4. CONCLUSION

The authors have proposed an ARMA based speech coding method with a new excitation signal model. An improved ARMA analysis has been developed. This analysis is based on LPC analysis and spectral inversion, in other words, zero to pole conversion, hence, it requires less computation, since the FFT algorithm and LPC analysis can be directly utilized. The MA parameter's misestimations are avoided by eliminating the spectral harmonic structure within the AR residual signal. The excitation signal is modeled as a pulse train whose density is varied subframe by subframe depending on the residual signal's power. The amplitudes of the pulse train are analytically solved to minimize the perceptually weighted errors between the original and synthetic signals. The subjective speech quality of the coder was comparable to that of 6-bit log PCM from an informal listening test's result.

Table 3 Coder's performance.

	Male 1	Male 2	Female 1	Female 3
SNRseg	15.6	14.3	15.7	15.3

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